



Reciprocating Compressor Monitoring with the Metrix 5580 / SW5580



Overview

This whitepaper examines the basis for condition monitoring on reciprocating compressors (hereafter referred to as simply “recips”), the classes of recips most often receiving condition monitoring, the need for more cost-effective solutions on a broader range of recip classifications, the suite of measurements recommended for adequate monitoring of the most common recip failure mechanisms, and the ways in which the Metrix 5580 / SW5580 family of products have been designed to economically address such applications.

Recips Versus Other Compressor Types

Reciprocating compressors are widely employed throughout industry; however, it

is well known that they incur a higher ratio of maintenance dollars per horsepower than their centrifugal or axial counterparts – in some cases as much as 400% more. This non-trivial difference in maintenance costs means that all else being equal, rotating machines would generally be preferred over reciprocating machines because the lifecycle costs are lower. However, all else is *not* equal and recips fit important niches in the compression universe where centrifugal and axials cannot be used at all, or at least not as efficiently. Examples include processes where extremely high compression ratios are required such as Low-Density Polyethylene (LDPE) production and/or processes where other compressor types cannot adequately handle the range of flow variation required.



Because reciprocating compressors are constant volume machines when there are not large variations in suction and/or discharge pressures, flow can be adjusted simply by changing the compressor speed. In contrast, speed adjustments in centrifugal and axial compressors can result in very poor efficiency or damaging aerodynamic instabilities such as surge. As such, reciprocating compressors will retain an indispensable niche in industrial process plants for the foreseeable future.

Packaged Versus API 618-Class Reciprocating Compressors

Given that reciprocating compressors incur substantially higher maintenance costs than their rotating counterparts, they are excellent candidates for condition monitoring, allowing the machine's measured condition to dictate necessary maintenance rather than frequent, highly invasive inspections based purely on running hours and OEM recommendations. Although it would be reasonable to conclude that a majority of reciprocating compressors thus have some type of installed condition monitoring system to help reduce these maintenance costs, the opposite is actually true: a small fraction of reciprocating compressors – only the most critical – are generally monitored today.

The class of machines most frequently monitored is characterized by the requirements of American Petroleum Institute Standard 618 which defines so-called “special purpose” reciprocating compressors built to specification for the end user as opposed to so-called “packaged” compressors. API 618 machines



Figure 1 – API 618 (top) and ISO 13631 (bottom) are well-known industry standards defining two different classes of reciprocating compressors

are usually large, employed in critical service, generally not 100% spared in the sense that loss of the machine substantially (if not fully) impacts production throughput, and mounted on a permanent foundation rather than a skid. This class of machine can justify even the most expensive systems because they are often deemed critical to the full production of a plant, such as hydrogen compression service in refineries. If one such machine goes down, millions of dollars per day in output is at stake, and the price of even the most expensive and expansive monitoring systems can be justified as they represent only a fraction of even a single day's production.

In contrast, this is not the case with smaller, less-critical reciprocating compressors, referred to above as "packaged" reciprocating compressors due to their packaged and often skid-mounted designs. Such machines are described in standards such as ISO 13631 and while machines of this class may play an important role in a plant or process, they typically do not have millions of dollars per day of revenue at stake and the implications of failure are thus not nearly so consequential as those of non-packaged machines in more critical service.

Cost Implications

Condition monitoring can demonstrably benefit almost all reciprocating compressors. It is thus important to distinguish here that the issue is not whether these smaller machines can benefit from condition monitoring; it is whether conventional condition monitoring solutions can be justified for such machines. Case in point: condition monitoring systems

designed primarily to address API 618-class machines often exceed an installed cost of \$100,000 throw. They were simply not designed to economically address these less-critical, packaged machines.

Unfortunately, solutions that simultaneously provided an adequate suite of measurements for these smaller reciprocating compressors while incurring more modest costs were not available. Industry responded most often by leaving these machines unmonitored. The monitoring that did exist was very often insufficient and consisted of rudimentary devices like eutectic switches to monitor piston rod drop, or mechanical vibration switches to monitor excessive casing vibration. Although such devices were relatively inexpensive, they offered no ability to observe trends, current readings relative to alarm setpoints, access to the raw signal for diagnostics and analytics, and other important factors. They were reactive in nature, not proactive, and could not reasonably be called condition monitoring solutions. They simply afforded basic machinery protection and were essentially "blind" devices.

Suitable Solutions

Metrix has historically filled an important niche in the machinery condition monitoring and protection market by offering cost-effective solutions suitable for less-critical machinery. Such machines do not require stringent adherence to industry standards such as API 670, suitable for only the most critical turbomachinery. They instead require systems with a feature set and corresponding price commensurate with the economics of the machine, the

service it provides, its failure mechanisms, and the consequences of failure.

The primary way in which Metrix addressed this niche was by pioneering the concept of “vibration transmitters” that convert the measured vibration signal amplitude from a sensor to a convenient 4-20mA proportional signal conforming to ISA SP50. This allowed the PLC, DCS, or other machinery control platform to act as the monitoring / trending / alarming / shutdown system. The PLC or DCS required only a standard analog input (i.e., 4-20mA) module and a discrete output (i.e., relay) module (see Figure 2). No longer was a special-purpose monitor required as the customer’s existing control system could be extended to accept vibration signals via the industry-standard 4-20mA interface. While vibration transmitters are suitable for many machine types, reciprocating compressors require a more specialized suite of measurements than can be addressed by conventional transmitter offerings. Metrix pioneered the transmitter types necessary for such solutions – namely, impact transmitters and rod drop transmitters.

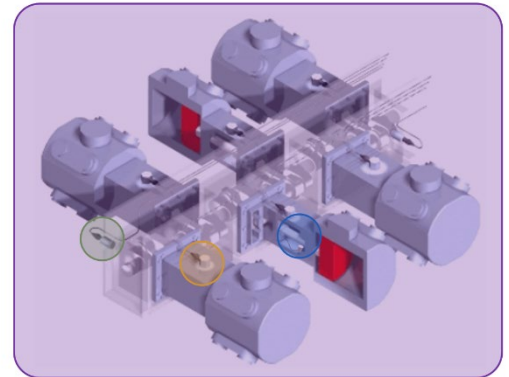


Figure 2 – A typical modern PLC (Modicon® M580) with analog input and discrete output modules in its three right-most slots.

However, these were inherently field devices, mounted on the machine, and while they worked well when properly installed and adjusted, they did not offer the convenience and features of monitoring systems that were software configurable and mounted in more accessible locations than the machine skid or even atop the compressor throws themselves. Also, the devices were not universal in nature. One model was required for vibration, another for position, another for rotative speed, and another for impact. The 5580 / SW5580 product family was introduced to provide a universal 2-channel device, software configurable for all necessary recip measurements and in an affordable, robust industrial package suitable for the global hazardous area classifications commonly encountered with recip instrumentation.

Where competing solutions are aimed primarily at API 618-class machines, the 5580 / SW5580 concerns itself with this smaller class of packaged machines and does so by reducing the cost of monitoring per throw by a factor of ten. Where it is not unusual to instrument 618 machines at costs exceeding \$100,000 per throw, operators of these smaller machines are looking for capable and reliable monitoring on the order of \$10,000 per throw. The 5580 / SW5580 has been designed with this price-point in mind and reflects a total installed cost of approximately \$3500 per measurement or about \$10,000 per throw for an adequately instrumented packaged machine compared with \$100,000 per throw for an adequately instrumented 618-class compressor. The suite of measurements recommended by Metrix on

Measurement Failure Mode	Rod Drop (MX2034 Transmitter, MX8030 Probe, MX8031 Cable)	XY Rod Position (MX2034 Transmitter, MX8030 Probe, MX8031 Cable)	Impact / Crosshead Acceleration (IT6810 Impact Transmitter)	Crankcase Velocity (ST5484E Velocity Transmitter)	Temperature: Suction Gas (DATAWATCH IX)	Temperature: Discharge Gas (DATAWATCH IX)	Temperature: Main Bearing (DATAWATCH IX)	Temperature: Valve (DATAWATCH IX)	Temperature: Crosshead Shoe (DATAWATCH IX)	Temperature: Packing (DATAWATCH IX)
Piston Rider Band Wear	X	X								
Piston Rod Bow		X								
Crosshead Shoe Vibration			X							
Piston Rod Nut Looseness		X	X							
Connecting Rod Looseness			X							
Loose Crosshead Guide Shims			X						X	
Main Bearing Failure							X			
Liquid in Cylinder			X	X						
Leaking Piston Rings						X				
Leaking Packing										X
Valve Leakage					X	X		X		
Overloading			X							



- Rod Drop / Rod Position
- Impact / Crosshead Acceleration
- Frame Vibration
- Temperature Monitoring

Figure 3A – Reciprocating Compressor

Figure 3B – Failure modes and corresponding measurements for reciprocating compressors

packaged compressors reflects experience gathered over several decades and this suite has shown to be adequate for detecting the most common malfunctions and maintenance-intensive aspects of the machine.

Figures 3A and 3B summarize these measurements and corresponding malfunctions detected. Figure 4 provides additional mounting location detail.

Later in this document, the attributes, features, and functions of the 5580 / SW5580 will be discussed in detail. Next, however, the measurements themselves are described along with their purpose.

Recip Measurements

Frame Vibration

Frame vibration (sometimes called crankcase velocity), is simply the overall vibration amplitude of the compressor frame. It is one of the most fundamental recip measurements and does not require special signal conditioning other than basic low-pass and high-pass filtering and signal integration (if the sensor does not provide a

native velocity output). Frame vibration is typically measured at two horizontal locations (each end of the frame). The horizontal mounting axis is chosen because the horizontal direction of the machine is usually the most compliant (i.e., least stiff). This measurement is useful for monitoring abnormalities that occur at or near the running speed of the machine and manifest as high casing vibration. Examples of such problems may include degradation of the machine's foundation, mechanical imbalance, or imbalance due to abnormal gas forces. Abnormalities in the running gear can also frequently manifest as elevated frame vibration.

The measurement is made with a conventional accelerometer (integrated to velocity units at the monitor) or with a sensor providing a native velocity output such as the Metrix SV6300 (piezo-velocity) or a suitable moving-coil velocity sensor. Piezo-velocity sensors are generally preferred as they have no moving parts that can wear out over time. A sensor frequency range and monitor passband that

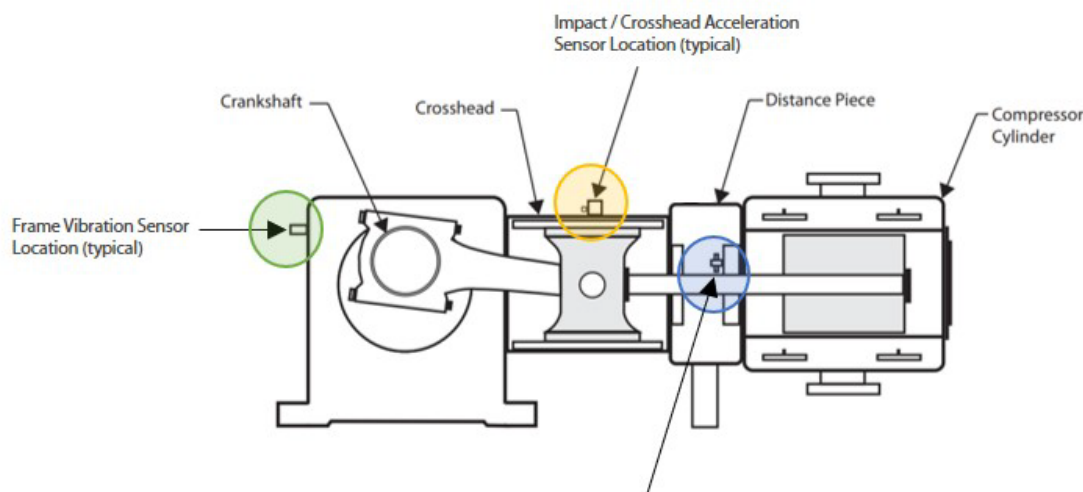


Figure 4 – Recommended Reciprocating Compressor Measurements and Locations

encompasses the running speed of the compressor is required.

Average Rod Drop

Rod drop is a measurement intended for horizontal cylinders with pistons utilizing non-metallic rider bands. As the rider bands wear, the gap between the piston and the bottom of the cylinder wall will decrease and the piston rod will exhibit a corresponding vertical drop in its average position. By mounting an eddy-current proximity probe vertically in the pressure packing case to observe the piston rod, this drop can be measured as a change in average gap (i.e. DC gap voltage) and using the geometry of the machine, the amount of drop in the rod can be translated to the amount of rider band wear. Alarms can be

set to notify operators and machinery personnel that it is time to replace the rider band(s). The probe can be mounted above or below the rod to observe this drop, but care must be taken to ensure probes mounted above the rod will remain within their usable linear range as the rod drops. For this reason, extended range probes (11mm tip diameter, or Metrix 8mm Extended Range feature) with 180 mils (4500 μm) of usable range are often selected.

It should be noted that not all reciprocating compressors are necessarily good candidates for rod drop measurements. Characteristics that compromise the rod drop measurement include, but are not limited to:

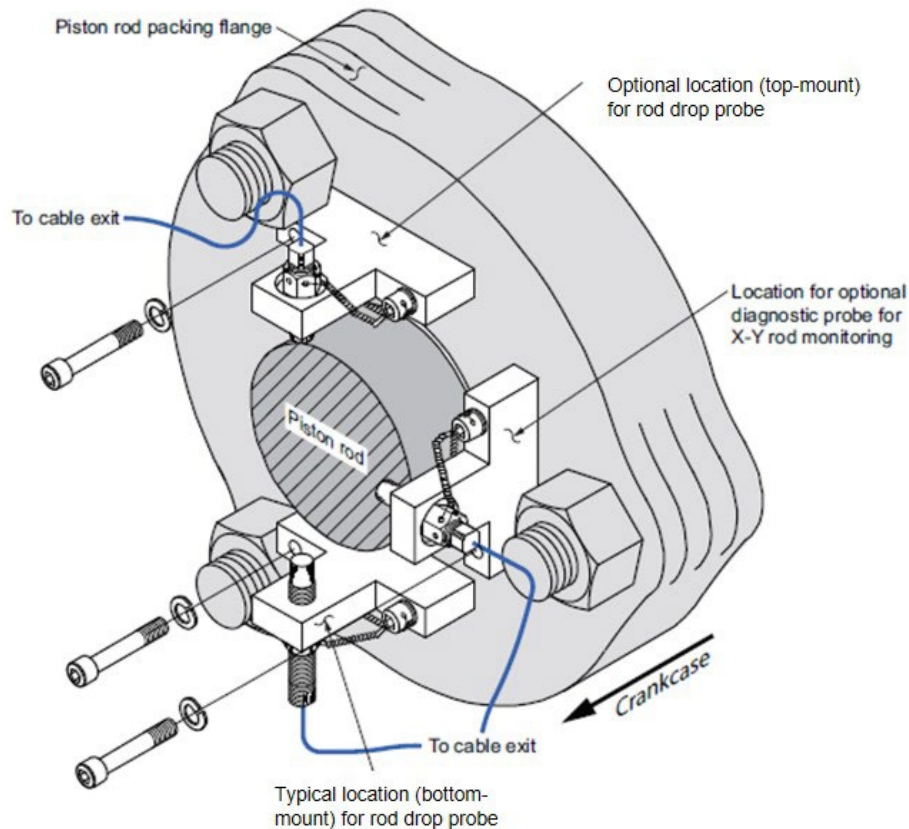


Figure 5 – Typical Rod Drop Probe Mounting Arrangement

- Non-lubricated cylinders
- Compressors with discharge pressures exceeding 2000 psi (13.79 MPa).
- Compressor frames rated more than 1000 kW (1 MW)
- Compressors with running speeds in excess of 1800 rpm
- Compressors with excessive flexing of piston rods; this can occur when the rod is too long relative to its girth and exhibits excessive flexure during the stroke, resulting in erratic measurements. A good rule of thumb is that the length of the piston rod should generally be no more than 25 times larger than the diameter of the piston rod.
- Other factors can also affect the efficacy of rod drop measurements as the above list does not comprise all relevant considerations. Contact the Metrix factory for a detailed application review before concluding that rod drop measurements will give satisfactory performance for your machine.

direction for additional diagnostic information on piston rod movement. This is depicted in Figure 5.

Impact

The impact transmitter was pioneered by Metrix in 2001 and a US patent¹ awarded in 2003. Impact has proven to be a remarkably effective measurement in the intervening two decades and many customers have adopted it so readily that they will not run their compressors without it. The concept is quite simple: by placing an accelerometer on (or near) the crosshead of each throw, looseness and other malfunctions in the running gear can manifest as mechanical impacts that excite resonances in the structure. Examples of malfunctions resulting in impacts include liquid in cylinders, excessive clearance in crosshead pin bushings, and loose or cracked nuts / cylinder liners / pistons.

The time waveform of these measurements exhibits a ringing and decay as the resonance is excited during each impact

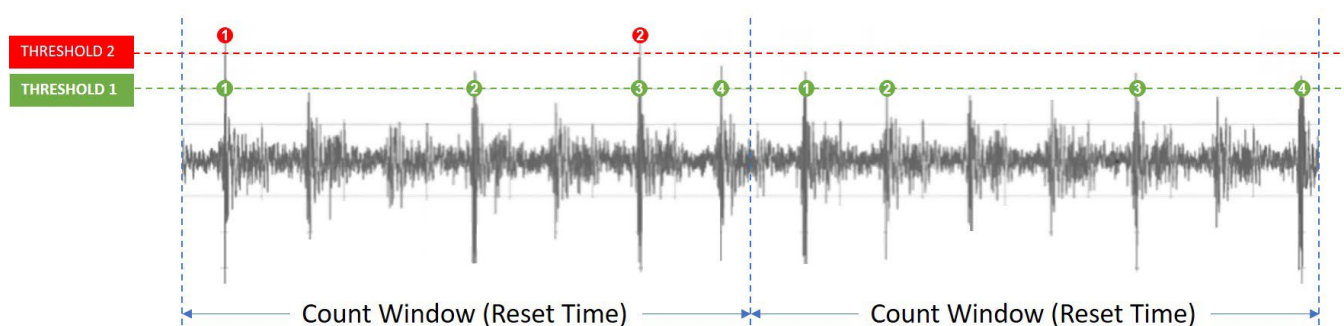


Figure 6 – Impact Measurements

If desired, a supplementary probe can also be mounted in the horizontal

direction for additional diagnostic information over a set period of time known as the “count window” or “reset time” is tallied. Once the

¹ US Patent 6,588,279 July 8, 2003 *Impact Transmitter for Reciprocating Machines*

time established for the count window has elapsed, the 5580 / SW5580 returns the number of impacts and then begins counting again. By trending this number, changes can be observed and alarms established to signify problems.

The period over which impacts are counted is usually selected to correspond to approximately 16 crank revolutions. For example, if a machine runs at 400 rpm, 16 crank revolutions spans 2.4 seconds and the reset time (count window) would be set accordingly as 2.4 seconds.

It is important to note that the absolute number of impacts occurring within the count window is not as important as the observable trend over minutes, hours, days, or longer. It is this trend that conveys the onset and growth of problems. The impact measurement has no associated engineering units. It is simply a count of events expressed as an integer value between 0 and 16. If more than 16 impacts occur during the count window, this generally means the threshold has been set too low or the impacting has progressed to levels that require analysis and maintenance intervention.

Referring again to Figure 6, using threshold 1 (green) would result in four impacts during the first and second count windows. Using threshold 2 (red) instead would yield two impacts during the first count window and no impacts during the second count window.

Please note that Figure 6 is intended to

convey the basic concept of impact measurements, threshold settings, and count window duration. It is not intended to serve as a comprehensive how-to guide for setting an appropriate threshold. For a more exhaustive and detailed treatment on establishing appropriate threshold level for impact measurements, refer to the installation manual for the 5580 / SW5580.

While the Metrix impact transmitter introduced an economical and effective means of monitoring numerous running gear issues on reciprocating compressors, its design suffers one drawback: it is cumbersome to adjust because the threshold and reset time settings are made on the transmitter itself, and the transmitter is mounted on the machine's crosshead (see Figure 7). This admittedly makes it difficult to work and make adjustments. Further, adjustments have to be made with the machine running. Because the transmitter is mounted on the throw's crosshead (or occasionally the distance piece), the service technician must be at the machine and sometimes even straddling the crosshead to make all



**Figure 7 – Metrix Impact Transmitter
Mounted on a Reciprocating Compressor**

adjustments. This is an undesirable environment for service personnel.

Impact monitoring via the 5580 / SW5580 is a dramatic improvement. First, it makes use of a standard accelerometer rather than a specialized transmitter for this measurement. The sensor type is less expensive and may be used elsewhere on the machine or in the plant for reduced spare parts requirements. Second, this arrangement places adjustment of threshold and count window settings in the 5580 / SW5580 itself – not the sensor. It thus removes service personnel from the machine location when configuring and making adjustments to the measurement chain and places them in a more suitable environment. This aspect alone makes impact monitoring via the 5580 / SW5580, rather than via a transmitter, a significant step forward.

Crosshead Acceleration

Closely related to the impact measurement is the crosshead acceleration measurement. This measurement uses the same accelerometer as that used for the impact measurement, but instead of counting impacts, it simply measures the 0-pk amplitude of the raw acceleration signal. It thus becomes a so-called “dual path” measurement where a single sensor goes through two signal processing paths: one to return impact counts and one to return the amplitude of the vibratory acceleration signal. This acceleration signal is useful for both alarming purposes and trending, and as a rich source of diagnostic information when connected to a suitable handheld analyzer. While changes in impact counts

signify *something* is malfunctioning, analysis of the raw acceleration signal yields insight into *what* is malfunctioning. A general rule-of-thumb is that no single crosshead should exhibit markedly more (i.e., twice as much) vibration than the others.

Vibration and Axial Position on Drivers

Many recips are electric motor driven. For those with rolling element bearings, an accelerometer or piezo-velocity sensor is often mounted on each bearing cap and brought into the 5580 / SW5580 as a seismic bearing vibration measurement. For drivers utilizing fluid-film bearings (whether electric motors, steam turbines, or others), proximity probes are used instead and are also compatible with the 5580 / SW5580 for both radial (shaft-relative vibration) and axial (thrust) measurements. As with all other measurements, alarms can be set (SW5580 only) and a 4-20mA output sent to a PLC, DCS, or other machine control platform for trending and display as part of an integrated machine control and monitoring environment.

Rotative Speed

While most machines will already have a speed measurement available, in the event one is not available, or a local display of speed is desired, the 5580 / SW5580 can be configured to display rotative speed from a proximity probe observing a toothed surface or a key / keyway.

Temperature

A variety of temperatures are useful for monitoring reciprocating compressor health. These include but are not limited to:

- Suction gas temperature

- Suction valve temperature
- Discharge gas temperature
- Discharge valve temperature
- Pressure packing case temperature
- Main bearing temperature
- Motor winding temperatures (usually six total: 2 TCs or 2 RTDs per winding on all three phases)

Most PLCs, DCSs, and machine control and automation platforms have suitable I/O modules to directly accept Resistance Temperature Detectors (RTDs) and/or thermocouples (TCs). These measurements can thus be introduced directly into the controller without need of a special signal conditioning device like the Metrix 5580 / SW5580. In the event that a control or automation platform cannot be used and a stand-alone monitoring and alarming device is required for temperature, the Metrix Datawatch IX (Figure 8) provides self-contained display, alarming with relay



Figure 8 – The Metrix Datawatch IX

outputs, trending, and Modbus digital communications for up to 8 inputs in a compact, cube-shaped package measuring less than 4 inches (102 mm) on each side. In addition to temperature inputs, the device can accept 4-20mA signals from pressure

transmitters, flow transmitters, and other field devices used in conjunction with reciprocating compressor control and monitoring.

Shutdown Versus Alarming Considerations

Two levels of setpoints are available in the SW5580: Alert (pre-shutdown) and Danger (shutdown). When the 5580 is used instead of the SW5580, the alarms are implemented in a PLC, DCS, or other control platform. Where alarm settings are available from the OEM, those levels should be implemented by default and then adjusted over time as process, operating conditions, and experience dictate. Although there can be numerous, vibration, position, and temperature measurements associated with reciprocating compressors, most industry standards suggest that only a small number be used for machinery protection (i.e. auto-shutdown) purposes with the rest being used for condition monitoring purposes. Most of the measurements discussed in this application note are suitable for both machinery protection purposes and condition monitoring purposes: frame vibration, crosshead acceleration, impact, rod drop, and vibration / position on the driving machine.

For measurements where proximity probes are used, whether rod drop on the compressor, axial position on the driver, or radial vibration on the driver, alarm setpoints are established based on the physical clearances in the bearings between shaft and bearing pads or the clearance

between piston and cylinder wall liner provided by rider bands.

In contrast, alarm limits from seismic transducers on the compressor do not derive from physical clearances and geometries of the machine but rather empirical data collected over time to distinguish normal operation from abnormal operation. Operators and maintenance personnel will quickly lose confidence in a system that generates spurious alarms, particularly when subsequent inspection shows no observable machine distress or damage.

Many temperature measurements are intended for auto-shutdown purposes, such as bearing temperatures, motor winding temperatures, lube oil temperatures (and pressures), and gas discharge temperatures. However, the control system for the compressor and its driver will often incorporate these critical temperature and pressure measurements as shutdown parameters. Examples include loss of lube oil pressure or excessive gas discharge temperature. For this reason, users will most often be dealing with vibration, position, and temperature measurements that did not come as part of the base control and protective package supplied by the compressor OEM. Valve temperature monitoring is one such example. It is not used for protective purposes and is instead used to indicate that the condition of one valve within a suction or discharge group is markedly different than its peers. As such, the valve temperature measurement computes the average temperature for a group of valves and alarms on the

differential between any single valve and this average. This can routinely be accomplished in the PLC or DCS. The Metrix Datawatch IX is also capable of such alarming.

Cylinder Performance Measurements

While the critical role that API 618 machines often play in a plant's production process justify the addition of cylinder pressure sensors and precision speed wheels for triggering measurements based on crank position to give rod load, rod reversal, and so-called PV (Pressure-Volume) curves as part of comprehensive cylinder performance monitoring, this level of condition monitoring is rarely warranted on less-critical classes of reciprocating compressors. Indeed, one of the primary distinctions between these reciprocating compressors and those for which the 5580 / SW5580 are intended is that such machines cannot justify the additional expense of continuous PV monitoring. The 5580/SW5580 product line thus does not have facilities for monitoring these parameters as they are not economically justifiable on machines of this class and are thus not discussed in this application note.

5580 Signal Conditioner & SW5580 Switch

The Metrix 5580 signal conditioner and SW5580 switch was designed to cost-effectively address machinery that does not warrant the cost and complexity of a system with all the features and functions required by API 670. It is a right-sized

solution for such machinery and offers an appropriate feature set

The following features make the devices appropriate for monitoring a wide variety of machinery employing both fluid-film and rolling element bearing types:

Integral Alarming / Relays

The 5580 and SW5580 differ only in that the SW version provides integral alarming capabilities and solid-state or electromechanical relays to externally announce and transmit these alarms for indication and machinery protection (i.e., auto-shutdown) purposes. The non-SW version is intended for installations where a PLC, DCS, or other control/automation platform is available for accepting the 4-20mA output of the 5580 and providing the alarming.

Universally Configurable Design

Prior generations of Metrix signal conditioners and switches consisted of different models for different measurements. One model was required for radial vibration measurements, another for axial position or rod drop measurements, another for impact measurements, another for speed, etc. In contrast, the 5580 uses a fully software configurable design² that allows it to be programmed for any measurement. This reduces personnel training costs and spare parts burdens. It also ensures that changes to measurements can be done entirely via software, in the

comfort and safety of an office environment, and then the device can be installed in the field.

Two-Channel Modularity

Prior Metrix signal conditioners and switches were single channel designs where two channels required twice as much space and twice as much hardware. The 5580 and SW5580 provide two independently configurable channels. For example, one channel can accept a proximity probe for axial position monitoring and the other channel can accept a seismic sensor for radial bearing vibration. The device can also be configured for so-called “dual-path” monitoring whereby a single sensor is processed in two separate paths to provide two separate measurements. For example, a single accelerometer mounted on a compressor throw’s crosshead can return the raw crosshead acceleration amplitude on one channel and impact counts on the other channel. Another example is a single proximity sensor monitoring piston rod position and vibration. Although the measurements share a common sensor, the signal processing, measurement types, and alarm setpoints are independent of one another.

The devices are also modular in that they can be supplied with only a single channel enabled and priced accordingly. The second channel can be enabled in the field, at a later date, using a special firmware key






² It is not possible to configure a 5580 Signal Conditioner as an SW5580 Switch, or to convert from solid-state relays to electromechanical relays in the field. The alarm processing circuitry and solid-state or electromechanical relays utilize different

circuit boards. If integral alarming is required immediately or is anticipated in the future, the SW model should be purchased with the appropriate type of relays.

supplied by the factory, eliminating the need to swap out two-channel hardware for one-channel hardware.

Multi-State LEDs

Alarm and status conditions are clearly annunciated at the device via multi-state LEDs as follows:

Color		5580	SW5580
Solid Green		Channel OK	Channel OK with no alarms
Flashing Yellow		N/A	Channel OK but in ALERT
Flashing Red		N/A	Channel OK but in DANGER
Solid Red		Channel NOT OK	Channel NOT OK
Off		Device unpowered	

There is one LED for each channel, allowing separate and unambiguous status annunciation for each measurement and sensor.

Universal Inputs

The 5580 and SW5580 support most commercially available acceleration, velocity, and proximity sensors, including the provision of any necessary sensor power. A single +24Vdc connection powers the device, its 4-20mA output(s), and its connected sensor(s) –including the -24Vdc power required by proximity transducers

```
CH 1      CH 2
14.56 mA  10.00 mA
1.32      6
g (pk)    impacts
```

and the constant current required by IEPE accelerometers and piezo-velocity sensors.

Integral 4-line, Dual-Channel OLED Display

The device's backlit OLED display ensures that readings are available locally rather than only at the HMI for the PLC, DCS, or other controller. Both channels are displayed continuously and simultaneously to include the channel number, the 4-20mA output value, the measured value, and the associated engineering units.

Individual, Configurable Relays

For the SW model, four (4) relays are provided, two for each channel. This allows ALERT and DANGER to be separately annunciated for each channel. The relays can be configured for latching or non-latching operation, normally energized or normally de-energized. Normally Open (N.O.) and Normally Closed (N.C.) wiring terminals are provided. Users can choose from either solid-state (SPST) or electromechanical (SPDT) relays at time of ordering. Solid-state relays are typically used for providing logic-level alarm status to controllers and other devices. Electromechanical relays are typically used to switch interposing relays, fuel valve solenoids, or other trip devices as part of the machine's control where the signal being switched is larger than a logic-level voltage.

Local Buffered Outputs

Conventional BNC connectors for each channel are provided for easy connection to portable instruments such as data collectors, DVMs, and analyzers where the cable length does not exceed 16 feet (5 meters). These outputs are isolated from

the 4-20mA outputs to ensure connection of external devices do not compromise the integrity of the monitoring or protective functions.

Amplified Buffered Outputs

When devices are mounted in junction boxes at the machine, it can be inconvenient to open the box to connect portable instruments. In prior generations of Metrix devices, and on most commercially available monitors, the buffered outputs are not suitable for wiring runs exceeding 5-10 meters without use of an external amplifier to drive the raw signals over long distances. The 5580 / SW5580 overcomes this limitation by employing integrated signal amplification, allowing buffered output signals to be driven up to 1000 feet (300 meters). The amplified signal is available at wiring terminals and is intended for permanent connection to remote patch panels or other condition monitoring systems.

NOT OK Annunciation

In addition to NOT OK status annunciation via the device's LEDs, the current loop (4-20mA) output for each channel will clamp to a value below 4mA, ensuring that a NOT OK condition can be distinguished from other conditions.

Condition	4-20mA output
No Power	0 mA
NOT OK	3.6 mA
OK, bottom scale	4 mA
OK, mid-range	Between 4 and 20 mA
OK, full scale	20 mA

Remote Reset

Latching-type alarms and relays can be reset remotely by using the reset terminal

on the device. Using "Reset" will release all cleared latched alarms.

USB Port

A USB port on the front of the device provides access to upload and download configuration via a connected computer running the 5580 configuration software. The port supports standard USB connections of up to 5m (16 feet).

Removable Wiring Terminal Blocks

For ease-of-maintenance, wiring terminals are removable. Four separate wiring terminal blocks are provided, two on top and two on bottom as follows:

Location	Connector #	Connections
Top	1	Channel 1 - I/O and Power
	2	Channel 1 – relays*
Bottom	3	Channel 2 - I/O and Reset*
	4	Channel 2 – relays*

* Only present on SW5580

DIN-rail Mounting

Each 5580 or SW5580 is mounted on standard 35mm DIN rail and uses an integral rail mounting clip.

Hazardous Area Approvals

The devices carry North American (CSA), European (ATEX), and Global (IECEx) hazardous area approvals, allowing them to be mounted in Division 2 / Zone 2 environments. Refer to Metrix drawings 1874437 for the 5580 and 1899690 for the SW5580. When the machine itself is in a Div 1 or Zone 0/1 environment, active or passive intrinsic safety barriers may be placed between the sensor and the 5580 to satisfy hazardous area approval criteria. The

5580 and corresponding I.S. barriers must be in a Div 2, Zone 2, or non-classified area. See the specific sensor drawing for I.S. barriers.

Typical System Arrangement

Figure 9 on the following page depicts a typical system arrangement for an electric motor driven 4-throw compressor comprising the following measurements:

- Rod Drop for each throw
- Crosshead acceleration for each throw
- Impact for each throw
- Frame Vibration (inboard and outboard) for the compressor frame
- Motor bearing vibration (inboard and outboard) assuming rolling element bearings on motor
- Motor speed

All inputs are shown. For clarity, outputs are shown for only a single 5580 / SW5580 and would be replicated for each device.

Power Supply Considerations

A 24Vdc power supply can be selected from any reputable provider and for added reliability, redundant schemes can be used if desired. When selecting a power supply, use the following sizing considerations for each 5580 / SW5580.

	5580	SW5580
Max Power Consumption	3.6 W	4.2 W

The table above assumes worst-case conditions where all relays are energized, all transducers are proximity probes consuming maximum power of 12mA @ 24V, all recorder outputs are at full scale of

20 mA, and all buffered outputs are driving the maximum allowable length of field wiring at maximum signal amplitude.

Enclosure Considerations

When mounting the system at the machine, a suitable enclosure is recommended to protect the electronics from the elements. Additionally, an enclosure may be mandatory for installation in CSA Class 1 Div 2, IECEx and ATEX Zone 2 hazardous environments. Where local display of status and current values is required, select an enclosure with a window.

When sizing the enclosure, refer to the 5580 / SW5580 datasheet (doc #1874512) for heat dissipation requirements to ensure adequate airflow and that temperature rise does not subject the devices to operation outside of maximum ratings. Make certain to include the power supply in these calculations as well. Consult the factory or your local Metrix sales professional for assistance, including installation and project advice.

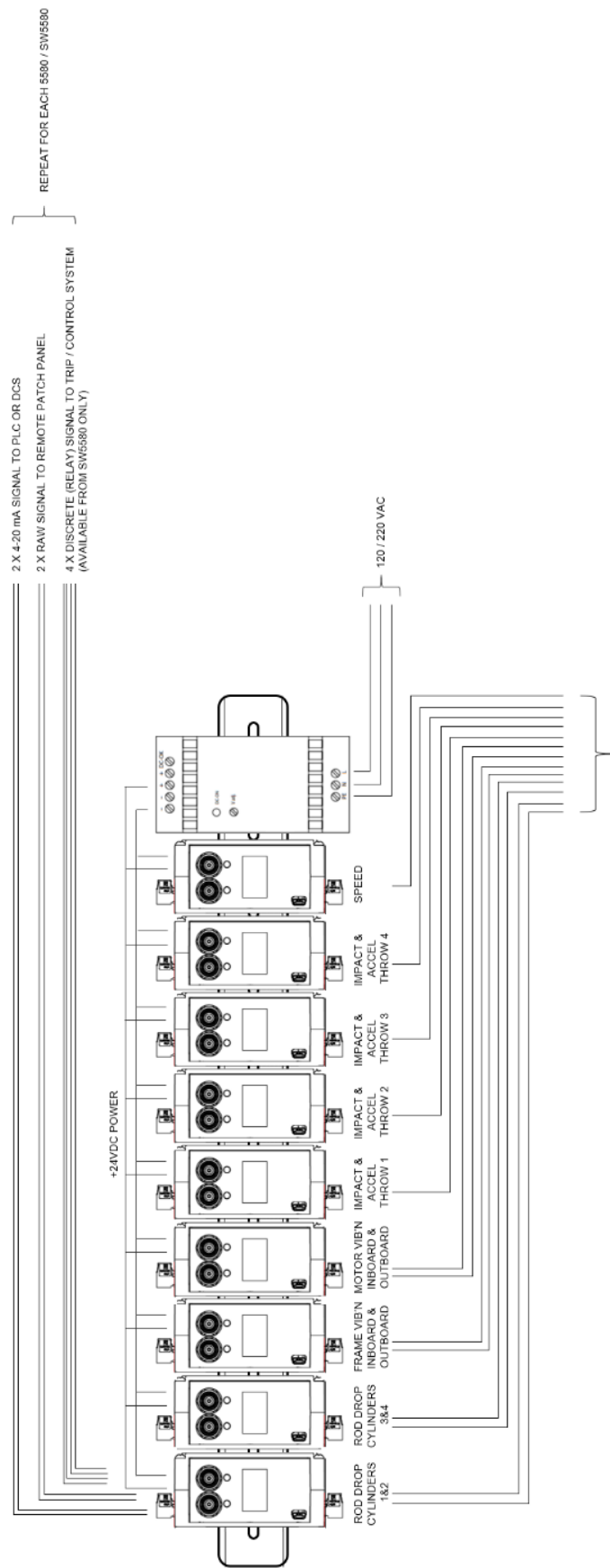
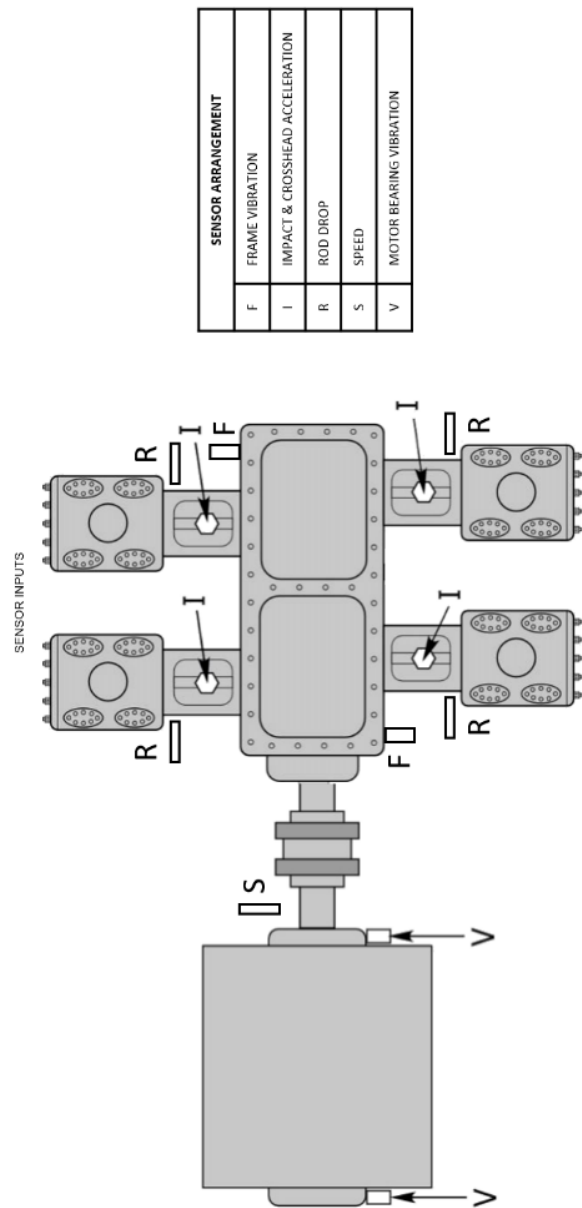


FIGURE 9 – Typical System Arrangement for 4-Throw Reciprocating Compressor



Note: Metrix is continuously improving our products. Please refer to our website to download the latest version of this whitepaper.

All trademarks, service marks, and/or registered trademarks used in this document belong to Metrix Instrument Company, L.P.

© 2024, Metrix Instrument Company, L.P. All rights reserved.